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Dispersion of Love wave in an isotropic layer sandwiched between orthotropic and prestressed inhomogeneous half-spaces

Abstract

An in-depth study has been carried out for the dispersion of Love waves in an isotropic elastic layer sandwiched between orthotropic and prestressed inhomogeneous elastic half-spaces. The inhomogeneities in density and rigidity of the lower half-space are space dependent and an arbitrary function of depth. Simple mathematical techniques are used to obtain dispersion relation for Love wave propagation in an isotropic layer. An extensive analysis is carried out through numerical computation to explore the effect of inhomogeneity and initial stress the lower half on the phase velocity of the Love waves. The numerical analysis of dispersion equation manifests that the phase velocity of the Love wave increases with the increase of stress parameter. The results further indicate that the inhomogeneity of the half space affect the wave velocity significantly. These results can be useful to study geophysical prospecting and understanding the cause and estimation of damage due to earthquakes.

Keywords

Love wave; initial stress; inhomogeneity; variable density.

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1 INTRODUCTION

The deformation at any point of the medium is useful to analyze the deformation field around mining tremors and drilling into the crust of the earth. It may also find application in various engineering problems, crystal physics and solid-earth geophysics regarding deformation of an anisotropic solid. In fact, study of surface waves in non-homogeneous and layered media has been of central interest to theoretical and experimental seismologists. Our Earth is a spherical and layered solid under high initial stress. Due to variation of temperature, gravitating pull, atmosphere, slow process of creep and pressure due to crustal layer, the critical initial stresses are stored in the layer of the Earth. At the present time the usefulness of dislocation theory in seismology is restricted by the absence of detailed knowledge of either the tectonic stress which drives the system or the stress which resists slip on the fault plane and by the absence of detailed observations of deformation preceding, accompanying of dislocation theory to seismology lie in the mathematical theory but

rather in the basis mechanics of faulting. The stresses which exist in an elastic body even though the external forces are absent are termed as prestresses. These stresses might exert significant effect on the elastic waves produced by earthquakes. The propagation of Love waves in a non-homogeneous elastic media is of considerable importance in earth-quake engineering and seismology on account of occurrence of non-homogeneities in the earth crust, as the earth is made up of different layers. The mathematical expression provides the bridge between modelling results and field applications.

Surface waves are very important in the study of earthquake engineering, geophysics and geodynamics. Love waves cause more destruction to the structure than that of the body waves due to its slower attenuation of the energy. The supplement of surface wave analysis and other wave propagation problems to anisotropic elastic materials has been the subject of many studies. Many authors have discussed Love wave propagation by considering various irregularities, inhomogeneities and boundaries of the Earth. Love (1944) and Ewing et al. (1957) proposed the propagation of waves in transversely isotropic medium. Chatopadhyay (1975) discussed Love waves due to irregularity in the thickness of the non- homogeneous crystal layer. Deresiewicz (1962) studied the propagation of Love waves in a homogeneous crust overlying an inhomogeneous substratum. Bhattacharya (1969) examined the Love waves in intermediate heterogeneous layer placed between isotropic elastic half-spaces. Midya (2004) discussed Love waves in micropolar homogeneous elastic media. Manna et al. (2013) discussed propagation of Love wave in hetrogeneous elastic half-space and piezoelectric layer. Du et al. (2008) studied the effect of initial stress on the propagation of piezoelectric layered structures loaded with viscous liquid. Liu and Wang (2005) studied Love waves in functionally graded layered piezoelectric structure. Chakraborty and Dey (1982) discussed the propagation of Love waves in water saturated soil underlain by heterogeneous elastic medium. Ke et al. (2005) discussed Love waves in nonhomogeneous fluid saturated porous layered half-space. Kundu et al. (2013) discussed propagation of Love wave in porous rigid layer kept over prestressed half space. Chattaraj et al. (2013) discussed Love wave propagation in irregular prestressed anisotropic porous stratum. Ghorai et al. (2010) showed the effect of rigid boundary on the propagation of Love wave in porous layer placed over an elastic half-space. Kadian and Singh (2010) studied the influence of size of barrier on Love wave reflection. Ahmed and Abd-Dahab (2010) studied the effect of initial stress on Love waves in an orthotropic Granular layer. Gupta et al. (2013) proposed a mathematical model to study Love wave propagation in homogeneous and initially stressed hetrogeneous half-spaces. Presently, Madan et al. (2014) investigated propagation of Love waves in saturated porous anisotropic layer. Kakar and Gupta (2014) studied Love waves in an intermediate heterogeneous layer lying in between homogeneous and inhomogeneous isotropic elastic half-spaces. More recently, Kundu et al. (2014a; 2014b) have examined Love wave propagation in fiber-reinforced media.

The present paper deals with the study of propagation of Love wave in a sandwiched layer lying between orthotropic and inhomogeneous half spaces. Five different cases have been studied for propagation of Love waves in a layer. The dispersion equations of Love waves under assumed conditions have been derived. Also numerical computation of dispersion equation has been performed to show the effect of initial stresses and inhomogeneity parameters on the propagation of Love waves. It has been found that initial stress parameter, rigidity parameter and density parameter of the lower half-space affect the phase velocity of Love waves.

2 FORMULATION OF THE PROBLEM

We have considered an isotropic and homogeneous layer of thickness H (denoted as M_2) sandwiched between two orthotropic and prestressed inhomogeneous (denoted as M_1 and M_3) half-spaces (as shown in Fig. 1). Let μ_2 and ρ_2 be the rigidity and density of the intermediate layer and rigidity and density in the upper half-space are μ_1 and ρ_1. The origin has been taken at the lower interface, Love wave propagates toward x-axis, while the positive z-axis toward the interior of the lower half space. The rigidity and density of the lower half are space dependent and an arbitrary function of depth i.e. $\mu_3 = \mu'(1+\varepsilon z)$ and $\rho_3 = \rho'(1+\varepsilon z)$. Here ε is the inhomogeneous parameter of lower half-space and having dimension that are inverse of length. Here ε is inhomogeneous parameter of lower half-space and having dimension that are inverse of length. The upper portion of superficial half-space corresponds to the free surface with zero relative density and rigidity as $\lim_{z\to-\infty} \mu_1 \to 0$ and $\lim_{z\to-\infty} \rho_1 \to 0$.

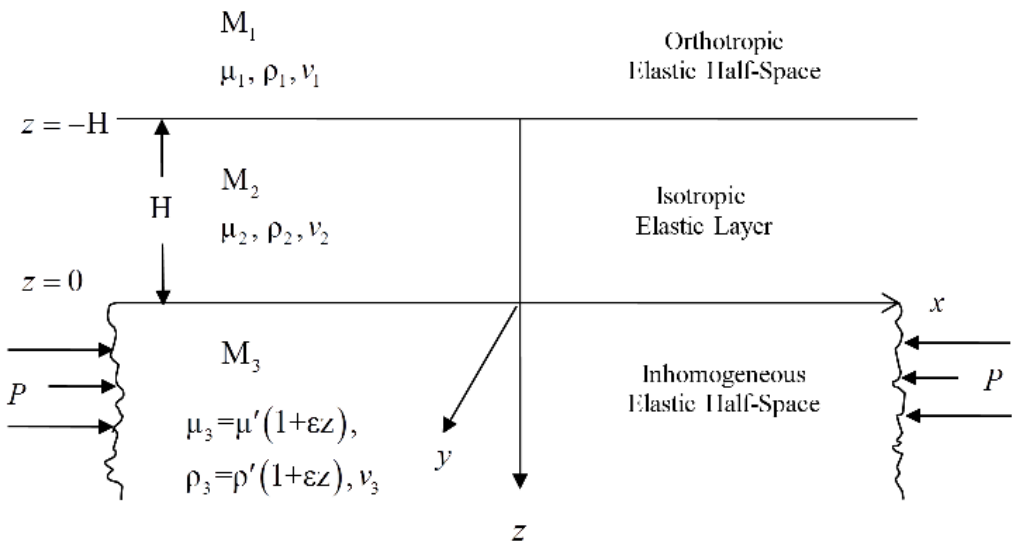

Figure 1: Geometry of the problem.

3 SOLUTION OF THE PROBLEM

3.1 Solution for the upper half-space

Equation of motion for upper half-space in the absence of body forces can be written as (Love, 1911)

$$\begin{aligned}
\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + \frac{\partial \tau_{xz}}{\partial z} &= \rho_1 \frac{\partial^2 u_1}{\partial t^2} \\
\frac{\partial \tau_{yx}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} + \frac{\partial \tau_{yz}}{\partial z} &= \rho_1 \frac{\partial^2 v_1}{\partial t^2} \\
\frac{\partial \tau_{zx}}{\partial x} + \frac{\partial \tau_{zy}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z} &= \rho_1 \frac{\partial^2 w_1}{\partial t^2}
\end{aligned} \tag{1}$$

where $\tau_{xx}, \tau_{xy}, \tau_{xz}, \tau_{yx}, \tau_{yy}, \tau_{yz}, \tau_{zx}, \tau_{zy}$ and τ_{zz} are the incremental stress components, u_1, v_1 and w_1 are the components of the displacement vector in the upper layer, ρ_1 is the density of the upper half-space.

The stress–strain relations are

$$\begin{aligned}
\tau_{xx} &= \mathrm{N}_{xx}e_{xx} + \mathrm{N}_{xy}e_{yy} + \mathrm{N}_{xz}e_{zz} \\
\tau_{xy} &= 2\mathrm{E}_z e_{xy} \\
\tau_{yy} &= \mathrm{N}_{yx}e_{xx} + \mathrm{N}_{yy}e_{yy} + \mathrm{N}_{yz}e_{zz} \\
\tau_{yz} &= 2\mathrm{E}_x e_{yz} \\
\tau_{zz} &= \mathrm{N}_{zx}e_{xx} + \mathrm{N}_{zy}e_{yy} + \mathrm{N}_{zz}e_{zz} \\
\tau_{zx} &= 2\mathrm{E}_y e_{zx}
\end{aligned} \tag{2}$$

where $\mathrm{N}_{xx}, \mathrm{N}_{xy}, \mathrm{N}_{xz}, \mathrm{N}_{yx}, \mathrm{N}_{yy}, \mathrm{N}_{yz}, \mathrm{N}_{zx}, \mathrm{N}_{zy}$ and N_{zz} are the incremental normal elastic coefficients, E_x, E_y and E_z shear modulus along x, y and z axis respectively. The strain components e_{xy}, e_{xx}, e_{yy}, e_{yz}, e_{zx} and e_{zz} are defined by

$$\begin{aligned}
&e_{xy} = \frac{1}{2}\left(\frac{\partial v_1}{\partial x} + \frac{\partial u_1}{\partial y}\right),\ e_{yz} = \frac{1}{2}\left(\frac{\partial w_1}{\partial y} + \frac{\partial v_1}{\partial z}\right),\ e_{zx} = \frac{1}{2}\left(\frac{\partial v_1}{\partial z} + \frac{\partial w_1}{\partial x}\right), \\
&e_{xx} = \left(\frac{\partial u_1}{\partial x}\right),\ e_{yy} = \left(\frac{\partial v_1}{\partial y}\right),\ e_{zz} = \left(\frac{\partial w_1}{\partial z}\right)
\end{aligned} \tag{3}$$

Using Love wave conditions $u_1 = w_1 = 0$, $v_1 = v_1(x,z,t)$ in equations (1) and (2), the equation of motion for the upper orthotropic half-space becomes

$$\mathrm{E}_z \frac{\partial^2 v_1}{\partial x^2} + \mathrm{E}_x \frac{\partial^2 v_1}{\partial z^2} = \rho_1 \frac{\partial^2 v_1}{\partial t^2} \tag{4}$$

and stress–strain relations reduces to

$$\begin{aligned}
&\tau_{xx} = \tau_{xy} = \tau_{xz} = \tau_{yy} = \tau_{zx} = \tau_{zy} = \tau_{zz} = 0 \\
&\tau_{yx} = 2\mathrm{E}_z e_{xy},\ \tau_{yz} = 2\mathrm{E}_x e_{yz}
\end{aligned} \tag{5}$$

To solve Eq. (4) we take the following substitution

$$v_1 = \mathrm{U(z)} \exp i(\omega t - kx) \tag{6}$$

where $\omega = kc$, c is phase velocity, $c_1 = \sqrt{\mu_1/\rho_1}$ and k is wave number.

Using Eq. (6) in Eq. (4), we get

$$\frac{\mathrm{d}^2\mathrm{U}(z)}{\mathrm{d}z^2} - \delta^2\mathrm{U}(z) = 0 \tag{7}$$

$$\text{where } \delta^2 = \frac{k^2}{\mathrm{E}_x}\left(\mathrm{E}_z - c^2\rho_1\right) \tag{8}$$

Therefore, the solution for the upper orthotropic half-space is given by

$$v_1 = \mathrm{A}\,\mathrm{e}^{\delta z}\exp i(\omega t - kx) \tag{9}$$

where A is arbitrary constant.

3.2 Solution for the lower half-space

Equation of motion for lower half-space under initial stress P acting along x-axis can be written as (Love, 1911)

$$\begin{aligned}
&\frac{\partial\sigma_{xx}}{\partial x} + \frac{\partial\sigma_{xy}}{\partial y} + \frac{\partial\sigma_{xz}}{\partial z} - P\left(\frac{\partial\Omega_z}{\partial y} - \frac{\partial\Omega_y}{\partial z}\right) = \rho_3\frac{\partial^2 u_3}{\partial t^2}\\
&\frac{\partial\sigma_{yx}}{\partial x} + \frac{\partial\sigma_{yy}}{\partial y} + \frac{\partial\sigma_{yz}}{\partial z} - P\left(\frac{\partial\Omega_z}{\partial x}\right) = \rho_3\frac{\partial^2 v_3}{\partial t^2}\\
&\frac{\partial\sigma_{zx}}{\partial x} + \frac{\partial\sigma_{zy}}{\partial y} + \frac{\partial\sigma_{zz}}{\partial z} - P\left(\frac{\partial\Omega_y}{\partial x}\right) = \rho_3\frac{\partial^2 w_3}{\partial t^2}
\end{aligned} \tag{10}$$

where $\sigma_{xx}, \sigma_{xy}, \sigma_{xz}, \sigma_{yx}, \sigma_{yy}, \sigma_{yz}, \sigma_{zx}, \sigma_{zy}$ and σ_{zz} are the incremental stress components, u_3, v_3 and w_3 are the components of the displacement vector and ρ_3 is the density of the lower half-space. Here, Ω_x, Ω_y and Ω_z are the rotational components in the lower half-space, which are defined by

$$\begin{aligned}
\Omega_x &= \frac{1}{2}\left(\frac{\partial w_3}{\partial y} - \frac{\partial v_3}{\partial z}\right)\\
\Omega_y &= \frac{1}{2}\left(\frac{\partial u_3}{\partial z} - \frac{\partial w_3}{\partial x}\right)\\
\Omega_z &= \frac{1}{2}\left(\frac{\partial v_3}{\partial x} - \frac{\partial u_3}{\partial y}\right)
\end{aligned} \tag{11}$$

Using Love wave conditions $u_3 = w_3 = 0$, $v_3 = v_3(x,z,t)$, Eq. (10) can be reduced to

$$\frac{\partial\sigma_{yx}}{\partial x} + \frac{\partial\sigma_{yz}}{\partial z} - \frac{P}{2}\left(\frac{\partial^2 v_3}{\partial x^2}\right) = \rho_3\frac{\partial^2 v_3}{\partial t^2} \tag{12}$$

The stress–strain relations are

$$\begin{aligned}\sigma_{xx} &= \sigma_{yy} = \sigma_{xz} = \sigma_{zz} = 0\\ \sigma_{yx} &= 2\mu_3 e_{xy} = 2\mu_3 \frac{1}{2}\left(\frac{\partial v_3}{\partial x} + \frac{\partial u_3}{\partial y}\right)\\ \sigma_{yz} &= 2\mu_3 e_{yz} = 2\mu_3 \frac{1}{2}\left(\frac{\partial w_3}{\partial y} + \frac{\partial v_3}{\partial z}\right)\end{aligned} \tag{13}$$

The inhomogeneity of rigidity and density of the lower half-space are

$$\mu_3 = \mu'\left(1+\varepsilon z\right),\ \rho_3 = \rho'\left(1+\varepsilon z\right) \tag{14}$$

Now, substituting the inhomogeneity of rigidity from Eq. (14) in Eq. (13), we have

$$\begin{aligned}\sigma_{yx} &= \mu'\left(1+\varepsilon z\right)\frac{\partial v_3}{\partial x}\\ \sigma_{yz} &= \mu'\left(1+\varepsilon z\right)\frac{\partial v_3}{\partial z}\end{aligned} \tag{15}$$

The equation of motion (12) with the help of equations (14) and (15) can be written as

$$\left(1-\frac{P}{2\mu'(1+\varepsilon z)}\right)\frac{\partial^2 v_3}{\partial x^2} + \frac{\partial^2 v_3}{\partial x^2} - \frac{\varepsilon}{1+\varepsilon z}\frac{\partial v_3}{\partial z} = \frac{\rho'}{\mu'}\frac{\partial^2 v_3}{\partial t^2} \tag{16}$$

To solve Eq. (16) we take the following substitution

$$v_3 = \mathrm{V(z)}\exp i(\omega t - kx) \tag{17}$$

Using Eq. (17) in Eq. (16), we get

$$\frac{\mathrm{d}^2\mathrm{V}(z)}{\mathrm{d}z^2} + \frac{\varepsilon}{1+\varepsilon z}\frac{\mathrm{dV}(z)}{\mathrm{d}z} + \left[\frac{\rho'}{\mu'}c^2 - \left(1-\frac{P}{2\mu'(1+\varepsilon z)}\right)\right]k^2\mathrm{V}(z) = 0 \tag{18}$$

Introducing $\mathrm{V}(z) = \Phi(z)\Big/\sqrt{\left(1+\varepsilon z\right)}$ into Eq. (18) to cancel the term $\mathrm{dV}(z)\big/\mathrm{d}z$, we have

$$\frac{\mathrm{d}^2\Phi(z)}{\mathrm{d}z^2} + \left[\frac{\varepsilon^2}{4\left(1+\varepsilon z\right)^2} - k^2\left[\left(1-\frac{P}{2\mu'(1+\varepsilon z)}\right) - \frac{c^2}{c_3^2}\right]\right]\Phi(z) = 0 \tag{19}$$

where c is phase velocity and $c_3 = \sqrt{\mu'\big/\rho'}$.

Introducing the non-dimensional quantities

$$r = \left[1 - \frac{P}{2\mu'(1+\varepsilon z)} - \frac{c^2}{c_3^2}\right]^{1/2} \quad , \; s = \frac{2rk(1+\varepsilon z)}{\varepsilon} \text{ and } \omega = kc$$

in Eq. (19), we get,

$$\frac{\mathrm{d}^2\Phi}{\mathrm{d}s^2} + \left(\frac{1}{4s^2} + \frac{s}{r} - \frac{1}{4}\right)\Phi(s) = 0 \tag{20}$$

Eq. (20) is the well known Whittaker's equation (Whittaker and Watson, 1990).

The solution Eq. (20) is given by

$$\Phi(s) = \mathrm{B}\, W_{r,0}(s) + \mathrm{B}_1 W_{-r,0}(-s) \tag{21}$$

where B and B_1 are arbitrary constants and $W_{r,0}(s)$, $W_{-r,0}(-s)$ are the Whittaker functions. Now considering the condition $\mathrm{V}(z) \to 0$ as $z \to \infty$ i.e. $\Phi(s) \to 0$ as $s \to \infty$ in Eq. (21), the exact solution becomes

$$\Phi(s) = \mathrm{B}\, W_{r,0}(s) \tag{22}$$

The solution of Eq. (22) is given by

$$v_3 = \mathrm{V(z)} \exp i(\omega t - kx) = \frac{\mathrm{B}\, W_{r,0}(s)}{\sqrt{(1+\varepsilon z)}} \exp i(\omega t - kx) \tag{23}$$

Eq. (23) is the displacement for the Love wave in the half space.

Now, expanding Eq. (23) up to linear term, we have

$$v_3 = \mathrm{B}\, \mathrm{e}^{\frac{-rk(1+\varepsilon z)}{\varepsilon}} \left(\frac{1}{\sqrt{(1+\varepsilon z)}} - \frac{\varepsilon}{8rk\sqrt{(1+\varepsilon z)}}\right) \exp i(\omega t - kx) \tag{24}$$

3.3 Solution for the intermediate isotropic layer

Equation of motion for intermediate layer can be written as (Love, 1911)

$$\begin{aligned}
\frac{\partial s_{xx}}{\partial x} + \frac{\partial s_{xy}}{\partial y} + \frac{\partial s_{xz}}{\partial z} &= \rho_2 \frac{\partial^2 u_2}{\partial t^2} \\
\frac{\partial s_{yx}}{\partial x} + \frac{\partial s_{yy}}{\partial y} + \frac{\partial s_{yz}}{\partial z} &= \rho_2 \frac{\partial^2 v_2}{\partial t^2} \\
\frac{\partial s_{zx}}{\partial x} + \frac{\partial s_{zy}}{\partial y} + \frac{\partial s_{zz}}{\partial z} &= \rho_2 \frac{\partial^2 w_2}{\partial t^2}
\end{aligned} \tag{25}$$

where s_{xx}, s_{xy}, s_{xz}, s_{yx}, s_{yy}, s_{yz}, s_{zx}, s_{zy} and s_{zz} are the incremental stress components, u_2, v_2 and w_2 are the components of the displacement vector and ρ_2 is the density of the intermediate layer.

The stress displacement relation for isotropic media is

$$s_{ij} = \lambda \, \mathrm{e} \, \delta_{ij} + 2\mu_2 e_{ij} \tag{26}$$

where λ and μ_2 are known as Lame's constants for homogeneous media, δ_{ij} is Kronecker delta and $e = \partial u_2 / \partial x + \partial v_2 / \partial y + \partial w_2 / \partial z$ is cubical dilatation. Here, $e_{ij} = \left(\partial u_i / \partial x_j + \partial u_j / \partial x_i \right) / 2$ where, u_i are the components of displacement vector and can be defined as

$$e_{xy} = \frac{1}{2}\left(\frac{\partial v_2}{\partial x} \right), \; e_{yz} = \frac{1}{2}\left(\frac{\partial v_2}{\partial z} \right), \; e_{zx} = e_{xx} = e_{yy} = e_{zz} = 0 \tag{27}$$

Using Love wave conditions $u_2 = w_2 = 0$, $v_2 = v_2(x, z, t)$, the stress–strain relations are

$$\begin{aligned} s_{xx} &= s_{yy} = s_{xz} = s_{zz} = 0 \\ s_{xy} &= \mu_2 \left(\frac{\partial v_2}{\partial x} \right) \\ s_{yz} &= \mu_2 \left(\frac{\partial v_2}{\partial z} \right) \end{aligned} \tag{28}$$

Using Eq. (28), the Eq. (25) can be written as

$$\frac{\partial^2 v_2}{\partial x^2} + \frac{\partial^2 v_2}{\partial z^2} = \frac{1}{c_2^2} \frac{\partial^2 v_2}{\partial t^2} \tag{29}$$

where $c_2 = \sqrt{\mu_2 / \rho_2}$.

To solve Eq. (29) we take the following substitution

$$v_2 = \mathrm{W(z)} \exp i(\omega t - kx) \tag{30}$$

where $\omega = kc$, c is phase velocity and k is wave number.

Using Eq. (30) in Eq. (29), we get

$$\frac{\mathrm{d}^2 \mathrm{W}(z)}{\mathrm{d}z^2} + \zeta^2 \mathrm{W}(z) = 0 \tag{31}$$

$$\text{where } \zeta^2 = k^2 \left(\frac{c^2}{c_2^2} - 1 \right) \tag{32}$$

Therefore, the solution for the intermediate layer is given by

$$v_2 = \left(\mathrm{C}\cos\zeta z + \mathrm{D}\sin\zeta z\right)\exp i(\omega t - kx) \tag{33}$$

where C and D are arbitrary constants.

4 BOUNDARY CONDITIONS

Both displacement and stress components are continuous at $z = 0$ and $z = -\mathrm{H}$, therefore the geometry of the problem leads to the following conditions:

1st Boundary conditions

(i) At the interface, $z = 0$ the continuity of the displacement along the x direction requires that $v_2 = v_3$, where v_2 and v_3 are the displacement components, along the y direction only, in the intermediate layer and lower half-space respectively.
(ii) At the interface, $z = 0$ the continuity of the stress requires that $\left(s_{yz}\right)_{\mathrm{M}_2} = \left(\sigma_{yz}\right)_{\mathrm{M}_3}$, where s_{yz} the relevant is stress component.
(iii) Also, stability conditions leads to $v_3 \to 0$ as $z \to +\infty$.

2nd Boundary conditions

(i) At the interface, $z = -\mathrm{H}$, the upper boundary plane is not free surface, the continuity of the displacement along the x direction requires that $v_1 = v_2$, where v_1 is the displacement component in the upper half-space along the y direction only.
(ii) At the interface, $z = -\mathrm{H}$, the continuity of the stress requires that $\left(\tau_{yz}\right)_{\mathrm{M}_1} = \left(s_{yz}\right)_{\mathrm{M}_2}$, where τ_{yz} the relevant is stress component.
(iii) Also, stability conditions leads to $v_1 \to 0$ as $z \to -\infty$.

5 DISPERSION RELATIONS

Applying 2nd boundary conditions in equations (2), (28) and equations (9), (33), we have

$$-\mathrm{A}\left(\frac{\mathrm{E}_x\delta\,\mathrm{e}^{-\delta\mathrm{H}}}{\mu_2\zeta}\right) + \mathrm{C}\sin\left(\zeta\mathrm{H}\right) + \mathrm{D}\cos\left(\zeta\mathrm{H}\right) = 0 \tag{34}$$

$$\mathrm{A}\,\mathrm{e}^{-\delta\mathrm{H}} - \mathrm{C}\cos\left(\zeta\mathrm{H}\right) + \mathrm{D}\sin\left(\zeta\mathrm{H}\right) = 0 \tag{35}$$

Now, applying 1st boundary conditions in equations (15), (28) and equations (24), (33), we have

$$\mathrm{D} - \mathrm{B}\frac{\mu'}{\mu_2}e^{-\frac{kr}{\varepsilon}}\sqrt{\frac{2kr}{\varepsilon}}\left(\frac{kr}{\varepsilon}+1\right)kr\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1} - 1\right\} = 0 \tag{36}$$

$$\mathrm{C}-\mathrm{B}e^{-\frac{kr}{\varepsilon}}\sqrt{\frac{2kr}{\varepsilon}}\left(\frac{kr}{\varepsilon}+1\right)=0 \tag{37}$$

Eliminating A, B, C and D from equations (34) to (37), the dispersion relation for Love waves can be calculated as

$$\begin{aligned}
&\left[\left\{\frac{\mathrm{E}_x\mu'\delta}{\mu_2^2\zeta^2}\mathrm{e}^{-\delta\mathrm{H}}e^{-\frac{kr}{\varepsilon}}\right\}\sqrt{\frac{2kr}{\varepsilon}}\left\{\frac{kr}{\varepsilon}+1\right\}(kr)\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}\right]\sin(\zeta\mathrm{H})+\\
&+\left[\left\{\frac{\mu'}{\mu_2\zeta}\mathrm{e}^{-\delta\mathrm{H}}e^{-\frac{kr}{\varepsilon}}\sqrt{\frac{2kr}{\varepsilon}}\right\}\left\{\frac{kr}{\varepsilon}+1\right\}(kr)\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}\right]\cos(\zeta\mathrm{H})+\\
&-e^{-\frac{kr}{\varepsilon}}\sqrt{\frac{2kr}{\varepsilon}}(kr)\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}\left\{\frac{\mathrm{E}_x\delta}{\mu_2\zeta}\mathrm{e}^{-\delta\mathrm{H}}\cos(\zeta\mathrm{H})-\mathrm{e}^{-\delta\mathrm{H}}\sin(\zeta\mathrm{H})\right\}=0
\end{aligned}$$

On solving further above equation, we get

$$\begin{aligned}
&\left[\left\{\frac{\mathrm{E}_x\mu'\delta}{\mu_2^2\zeta^2}\mathrm{e}^{-\delta\mathrm{H}}e^{-\frac{kr}{\varepsilon}}\sqrt{\frac{2kr}{\varepsilon}}\right\}\left\{\frac{kr}{\varepsilon}+1\right\}(kr)\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}\right]\tan(\zeta\mathrm{H})+\\
&+\left[\left\{\frac{\mu'}{\mu_2\zeta}\mathrm{e}^{-\delta\mathrm{H}}e^{-\frac{kr}{\varepsilon}}\sqrt{\frac{2kr}{\varepsilon}}\right\}\left\{\frac{kr}{\varepsilon}+1\right\}(kr)\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}\right]+\\
&-\frac{\mathrm{E}_x\delta}{\mu_2\zeta}\mathrm{e}^{-\delta\mathrm{H}}e^{-\frac{kr}{\varepsilon}}\sqrt{\frac{2kr}{\varepsilon}}(kr)\left(\frac{kr}{\varepsilon}+1\right)+\mathrm{e}^{-\delta\mathrm{H}}e^{-\frac{kr}{\varepsilon}}\sqrt{\frac{2kr}{\varepsilon}}(kr)\left(\frac{kr}{\varepsilon}+1\right)\tan(\zeta\mathrm{H})=0
\end{aligned}$$

which implies

$$\begin{aligned}
&\mathrm{e}^{-\delta\mathrm{H}}e^{-\frac{kr}{\varepsilon}}\left\{\frac{kr}{\varepsilon}+1\right\}\left\{\sqrt{\frac{2kr}{\varepsilon}}\right\}\left[\frac{\mathrm{E}_x\mu'\delta}{\mu_2^2\zeta^2}(kr)\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}+1\right]\tan(\zeta\mathrm{H})+\\
&+\frac{1}{\mu_2\zeta}\mathrm{e}^{-\delta\mathrm{H}}e^{-\frac{kr}{\varepsilon}}\left\{\sqrt{\frac{2kr}{\varepsilon}}\right\}\left(\frac{kr}{\varepsilon}+1\right)\left[\left\{\mu'\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}-\mathrm{E}_x\delta\right]=0
\end{aligned} \tag{38}$$

On solving further equation (38), we get

$$\tan(\zeta\mathrm{H})=\frac{\mu_2\zeta\left[\mathrm{E}_x\delta+\mu'(kr)\left\{1-\left(\frac{kr}{\varepsilon}+1\right)^{-1}\right\}\right]}{\mu'\mathrm{E}_x\delta(kr)\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}+\mu_2^2\zeta^2}$$

which implies

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}kH\right)=\frac{\mu_2 k\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}\left[E_x k\sqrt{\frac{1}{E_x}\left[E_z-c^2\rho\right]}+\mu' kr\left\{1-\left(\frac{kr}{\varepsilon}+1\right)^{-1}\right\}\right]}{\mu' E_x k^2 r\sqrt{\frac{1}{E_x}\left[E_z-c^2\rho\right]}\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}+\mu_2^2 k^2\left(\frac{c^2}{c_2^2}-1\right)}=$$

$$=\frac{\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}\left[E_x\sqrt{\frac{E_z}{E_x}\left[1-\frac{c^2\rho}{E_z}\right]}+\mu' r\left\{1-\left(\frac{kr}{\varepsilon}+1\right)^{-1}\right\}\right]}{\mu' E_x r\sqrt{\frac{E_z}{E_x}\left[1-\frac{c^2\rho}{E_z}\right]}\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}+\mu_2^2\left(\frac{c^2}{c_2^2}-1\right)}$$

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}kH\right)=\frac{E_x\sqrt{\frac{E_z}{E_x}\left[1-\frac{c^2\rho}{E_z}\right]}+\mu' r\left\{1-\left(\frac{kr}{\varepsilon}+1\right)^{-1}\right\}}{\mu' E_x r\sqrt{\frac{E_z}{E_x}\left[1-\frac{c^2\rho}{E_z}\right]}\left\{\left(\frac{kr}{\varepsilon}+1\right)^{-1}-1\right\}+\mu_2^2\left(\frac{c^2}{c_2^2}-1\right)}\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)} \tag{39}$$

Eq. (39) is dispersion relation of Love waves in an intermediate isotropic vertical layer placed in between orthotropic and prestressed inhomogeneous half-spaces.

Special cases

Case 1 If $E_x \to E_z \to \mu_1$, the Eq. (39) reduces to

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}kH\right)=\frac{\mu_1\sqrt{\left(1-\frac{c^2}{c_1^2}\right)}+\mu' r\left\{1-\left(\frac{kr}{\varepsilon}+1\right)^{-1}\right\}}{\mu_2^2\left(\frac{c^2}{c_2^2}-1\right)-\mu'\mu_1 r\sqrt{\left(1-\frac{c^2}{c_1^2}\right)}\left\{1-\left(\frac{kr}{\varepsilon}+1\right)^{-1}\right\}}\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)} \tag{40}$$

Eq. (40) is dispersion relation of Love waves in an intermediate isotropic vertical layer placed in between homogeneous and prestressed inhomogeneous half-spaces.

Case 2 If $\varepsilon \to 0$, the Eq. (39) reduces to

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}kH\right)=\frac{E_x\sqrt{\frac{E_z}{E_x}\left[1-\frac{c^2\rho}{E_z}\right]}+\mu'\left[1-\frac{P}{2\mu'}-\frac{c^2}{c_3^2}\right]^{\frac{1}{2}}}{\mu_2^2\left(\frac{c^2}{c_2^2}-1\right)-\mu' E_x\left[1-\frac{P}{2\mu'}-\frac{c^2}{c_3^2}\right]^{\frac{1}{2}}\sqrt{\frac{E_z}{E_x}\left[1-\frac{c^2\rho}{E_z}\right]}}\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)} \tag{41}$$

Eq. (41) is dispersion relation of Love waves in an intermediate isotropic vertical layer placed in between orthotropic and prestressed homogeneous half-spaces.

Case 3 If $\mathrm{E}_x \to \mathrm{E}_z \to \mu_1,\ \varepsilon \to 0$ the Eq. (39) reduces to

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}k\mathrm{H}\right)=\frac{\mu_1\sqrt{1-\frac{c^2}{c_1^2}}+\mu'\left[1-\frac{P}{2\mu'}-\frac{c^2}{c_3^2}\right]^{\frac{1}{2}}}{\mu_2^2\left(\frac{c^2}{c_2^2}-1\right)-\mu'\mu_1\left[1-\frac{P}{2\mu'}-\frac{c^2}{c_3^2}\right]^{\frac{1}{2}}\sqrt{1-\frac{c^2}{c_1^2}}}\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)} \tag{42}$$

Eq. (42) is dispersion relation of Love waves in an intermediate isotropic vertical layer placed in between homogeneous and prestressed homogeneous half-spaces.

Case 4 If $\varepsilon \to 0,\ P \to 0$, the Eq. (39) reduces to

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}k\mathrm{H}\right)=\frac{\mathrm{E}_x\sqrt{\frac{\mathrm{E}_z}{\mathrm{E}_x}\left[1-\frac{c^2\rho}{\mathrm{E}_z}\right]}+\mu'\left[1-\frac{c^2}{c_3^2}\right]^{\frac{1}{2}}}{\mu_2^2\left(\frac{c^2}{c_2^2}-1\right)-\mu'\mathrm{E}_x\left[1-\frac{c^2}{c_3^2}\right]^{\frac{1}{2}}\sqrt{\frac{\mathrm{E}_z}{\mathrm{E}_x}\left[1-\frac{c^2\rho}{\mathrm{E}_z}\right]}}\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)} \tag{43}$$

Eq. (43) is dispersion relation of Love waves in an intermediate isotropic vertical layer placed in between orthotropic and homogeneous half-spaces.

Case 5 If $\mathrm{E}_x \to \mathrm{E}_z \to \mu_1,\ \varepsilon \to 0,\ P \to 0$, the Eq. (39) reduces to

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}k\mathrm{H}\right)=\frac{\mu_1\sqrt{1-\frac{c^2}{c_1^2}}+\mu'\left[1-\frac{c^2}{c_3^2}\right]^{\frac{1}{2}}}{\mu_2^2\left(\frac{c^2}{c_2^2}-1\right)-\mu'\mu_1\left[1-\frac{c^2}{c_3^2}\right]^{\frac{1}{2}}\sqrt{1-\frac{c^2}{c_1^2}}}\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)} \tag{44}$$

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}k\mathrm{H}\right)=\frac{\mu'\sqrt{\left(1-\frac{c^2}{c_3^2}\right)}}{\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}} \tag{45}$$

Also, on neglecting the lower half space, Eq. (44) reduces to

$$\tan\left(\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}k\mathrm{H}\right)=\frac{\mu_1\sqrt{\left(1-\frac{c^2}{c_1^2}\right)}}{\mu_2\sqrt{\left(\frac{c^2}{c_2^2}-1\right)}} \tag{46}$$

Eq. (45) and Eq. (46) are classic Love wave dispersion relation; hence it validates our solution for Love waves in an intermediate isotropic vertical layer placed in between orthotropic and prestressed inhomogeneous half-spaces.

6 NUMERICAL CALCULATIONS AND DISCUSSION

To show the effect of inhomogeneity parameters and initial stress parameters of lower half-space on Love wave propagation in intermediate layer, we take following parameters Gubbins (1990).

(i) Material Parameters for upper half-space.

$$\mathrm{E}_x = 5.65\text{x}10^{10}\ \mathrm{N/m^2},\ \mathrm{E}_z = 2.46\text{x}10^{10}\ \mathrm{N/m^2},\ \rho_1 = 7800\ \mathrm{kg/m^3}.$$

(ii) Material Parameters for intermediate layer.

$$\mu_2 = 5.82\text{x}10^{10}\ \mathrm{N/m^2},\ \rho_2 = 4500\ \mathrm{kg/m^3}.$$

(iii) Material Parameters for lower half-space.

$$\mu_3 = 6.34\text{x}10^{10}\ \mathrm{N/m^2},\ \rho_3 = 3364\ \mathrm{kg/m^3}.$$

We have plotted dimensionless phase velocity c/c_2 against dimensionless wave number kH for Eq. (39) using MATLAB software. The effects of initial stress parameters $P/(2\mu')$ and inhomogeneity parameters ε/k on Love wave propagation have been shown in Figs. 2–4. Figure 2 is plotted for dimensionless phase velocity c/c_2 in intermediate layer against dimensionless wave number kH of Love wave for different values of inhomogeneity parameter ε/k and in the presence of constant initial stress parameter $P/(2\mu') = 0.5$ present in the lower half-space. It is clear from this figure, the phase velocity increases with increase of inhomogeneity parameters ε/k. Figure 3 represents the variation of dimensionless phase velocity c/c_2 in intermediate layer against dimensionless wave number kH of Love wave for different values of initial stress parameter $P/(2\mu')$ and in the presence of constant inhomogeneity parameter $\varepsilon/k = 0.5$ present in the lower half-space. The values of stress parameters for curves have been taken as 0.0, 0.3, 0.5 and 0.7, respectively. It is observed from these curves that as the stress parameters in the half-space increases, the velocity of Love wave increases. Figure 4 shows the effect of initial stress parameters on dimensionless phase velocity c/c_2 in intermediate layer against dimensionless wave number kH of Love wave in the presence of constant inhomogeneity parameter for homogeneous media. From above numerical analysis, the following observations are made:

i. In entire figures, dimensionless phase velocity c/c_2 of Love waves in intermediate layer decreases with increase of dimensionless wave number kH.
ii. The dimensionless phase velocity c/c_2 of Love wave in intermediate layer shows remarkable change with inhomogeneity ε/k and stress parameters $P/(2\mu')$.
iii. It is observed as the depth increases the velocity of Love wave in intermediate layer decreases.
iv. The phase velocity c/c_2 of Love wave in intermediate layer decreases with the decrease of initial stress $P/(2\mu')$ of lower half-space.
v. The phase velocity c/c_2 of Love wave in intermediate layer increases with the increase of inhomogeneity parameter ε/k of lower half-space.

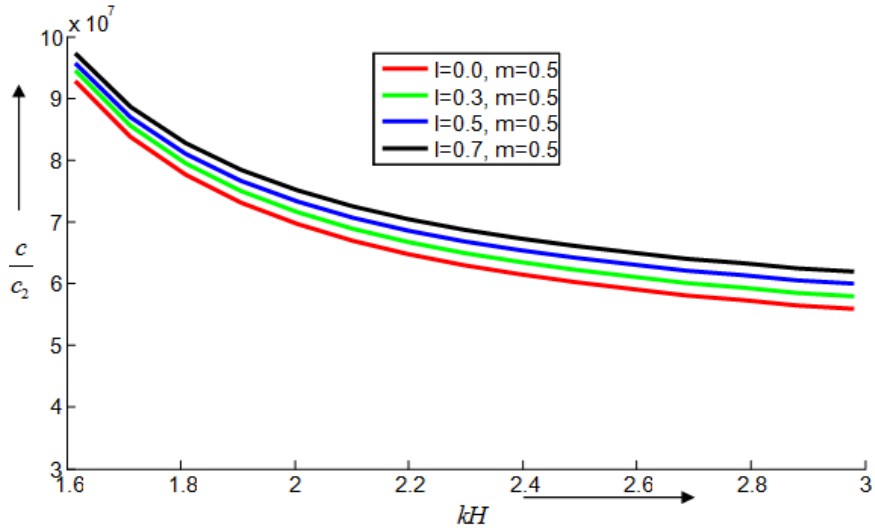

Figure 2: Dimensionless phase velocity c/c_2 in intermediate layer against dimensionless wave number kH of Love wave for different values of inhomogeneity parameter $l = \varepsilon/k$ and in the presence of constant initial stress parameter $m = P/(2\mu') = 0.5$ present in the lower half-space.

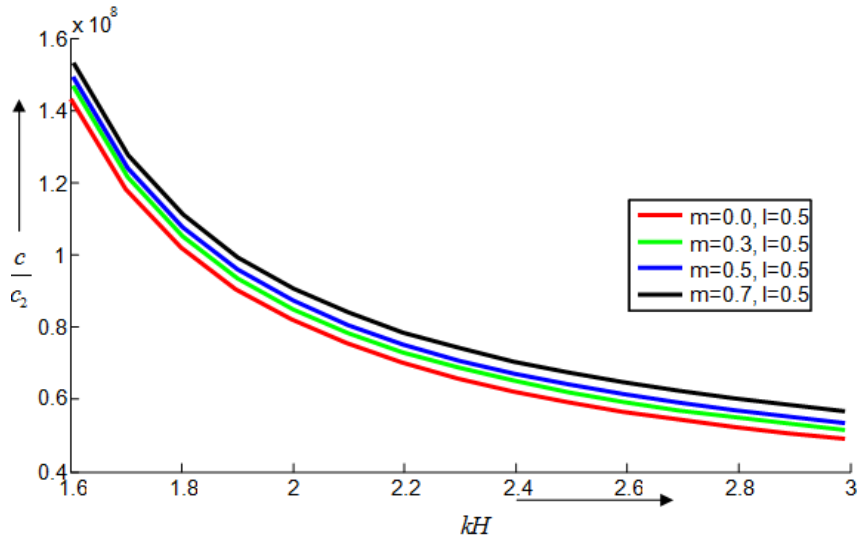

Figure 3: Dimensionless phase velocity c/c_2 in intermediate layer against dimensionless wave number kH of Love wave for different values of initial stress parameter $m = P/(2\mu')$ and in the presence of constant inhomogeneity parameter $l = \varepsilon/k = 0.5$ present in the lower half-space.

7 CONCLUSIONS

In this paper, an analytical approach is used to investigate the propagation of Love wave in a homogeneous isotropic layer of finite thickness between orthotropic and inhomogeneous half spaces. It has been observed that present geometry allows Love waves to propagate. Implicit dispersion relation and closed form solutions for displacement in the layer and half-spaces have been obtained. The significant effect of inhomogeneity parameters and stress parameters on Love wave propagation

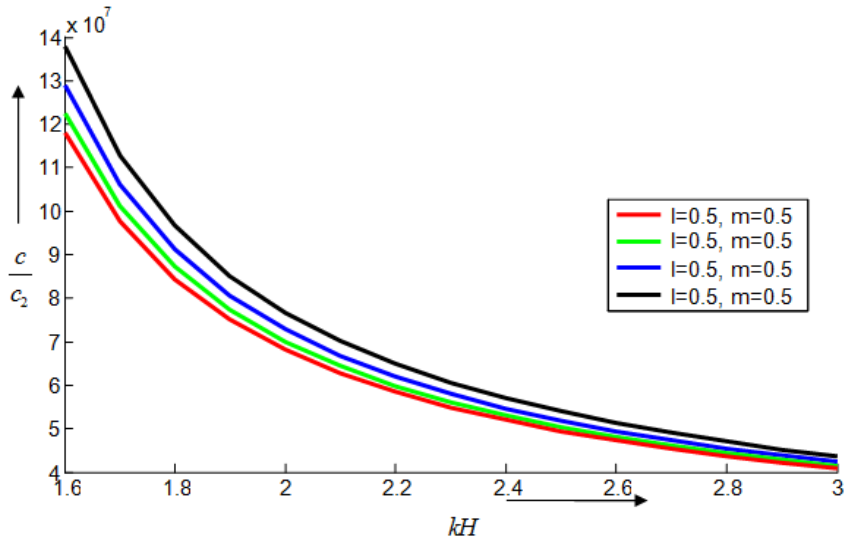

Figure 4: Dimensionless phase velocity c/c_2 in intermediate layer against dimensionless wave number kH of Love wave for different values of initial stress parameter $m = P/(2\mu')$ and in the presence of constant inhomogeneity parameter $l = \varepsilon/k$ for homogeneous media.

has been observed. Phase velocity has been also computed numerically, and the effects of variation in density and rigidity in the lower half-space have been studied. It has been investigated that the initial stresses have a pronounced effect on the propagation of Love waves. In special cases, when the intermediate layer and lower half-space or intermediate layer and upper half-space are homogeneous, our computed equation coincides with the classical equation of Love wave. Since Earth is an initially stressed, orthotropic and can be considered as composed of different inhomogeneous layers, hence, it is more realistic to consider the inhomogeneity and initial stress discussed in the present problem to study the propagation of Love waves in prestressed inhomogeneous Earth medium. The present study may be useful for geophysical applications of propagation of Love waves in different layers of Earth.

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